

Data Acquisition And Injury Calculation

Crash Protection

Technical Bulletin CP 005

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PREFACE

During the test preparation, vehicle manufacturers are encouraged to liaise with the laboratory and to check that they are satisfied with the way cars are set up for testing. Where a manufacturer feels that a particular item should be altered, they should ask the laboratory staff to make any necessary changes. Manufacturers are forbidden from making changes to any parameter that will influence the test, such as dummy positioning, vehicle setting, laboratory environment etc.

It is the responsibility of the test laboratory to ensure that any requested changes satisfy the requirements of Euro NCAP. Where a disagreement exists between the laboratory and manufacturer, the Euro NCAP secretariat should be informed immediately to pass final judgment. Where the laboratory staff suspect that a manufacturer has interfered with any of the set up, the manufacturer's representative should be warned that they are not allowed to do so themselves. They should also be informed that if another incident occurs, they will be asked to leave the test site.

Where there is a recurrence of the problem, the manufacturer's representative will be told to leave the test site and the Secretary General should be immediately informed. Any such incident may be reported by the Secretary General to the manufacturer and the person concerned may not be allowed to attend further Euro NCAP tests.

DISCLAIMER: Euro NCAP has taken all reasonable care to ensure that the information published in this protocol is accurate and reflects the technical decisions taken by the organisation. In the unlikely event that this protocol contains a typographical error or any other inaccuracy, Euro NCAP reserves the right to make corrections and determine the assessment and subsequent result of the affected requirement(s).

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1 TEST DATA

A complete Euro NCAP assessment consists of many tests. To ensure consistency in the general folder structure, this chapter details the required folder structure. For each (sub)test where measurements are performed on dummies, vehicles or other test equipment, all test data needs to be provided in ISO-MME 1.6 format and needs to be fully compliant with the ISO/TS 13499 standard. It should be noted that some filenames are also prescribed in this document. All data shall be provided using SI units unless specified otherwise.

1.1 General test series folder structure

The following folder structure, generated automatically in the Euro NCAP sharing platform, is to be used for all test series where the name of the main folder containing all tests consists of:

- The year of test
- OEM abbreviation
- Euro NCAP internal number (4 digits)
- Make and Model

Where Euro NCAP tests contain a number of sub-tests, the next paragraph details the folder structure, names of the sub-system test folders and where applicable the filenames.

On the highest level, the folder structure is as follows with on the right an example using the Volvo XC90 that is assumed to be tested in 2026 with a Euro NCAP internal number of 9999.

MAIN FOLDER NAME	 26-VOL-9999-Volvo XC90 	Uploaded by:
Frontal MPDB test folder	26-VOL-9999-MP1	Laboratory
Frontal FW test folder	26-VOL-9999-FW1	Laboratory
Frontal Sled & VT test folder	26-VOL-9999-VTF	OEM
Side MDB test folder	26-VOL-9999-MD1	Laboratory
Side Pole test folder	26-VOL-9999-PO1	Laboratory
Far side test folder	26-VOL-9999-FAR	OEM
Knee mapping test folder	26-VOL-9999-KNE	OEM
Whiplash tests folder	26-VOL-9999-WHL	Laboratory
Child Occupant Protection folder	▶ 26-VOL-9999-COP	Laboratory
VRU test folder	26-VOL-9999-VRU	Laboratory
AEB Pedestrian test folder	26-VOL-9999-AEBP	Laboratory
AEB Bicyclist test folder	26-VOL-9999-AEBB	Laboratory
AEB Motorcyclist test folder	26-VOL-9999-AEBM	Laboratory
AEB Car-to-Car test folder	26-VOL-9999-AEBC	Laboratory
SAS tests folder	26-VOL-9999-SAS	Laboratory
LSS tests folder	26-VOL-9999-LSS	Laboratory
OSM test folder	26-VOL-9999-OSM	Laboratory
Inspection folder	26-VOL-9999-INS-lab name	Laboratory

Where a retest is performed, the identifier for that loadcase MP, FW etc. will have the lest digit increased by 1. For example MP2 etc.

1.1.1 MPDB sub-test folders

• MAIN FOLDER NAME

L ...

Frontal MPDB test number

Channel

Document

Movie

Photo

Report

Static

MME-file

1

• 26-VOL-9999-Volvo XC90

...

26-VOL-9999-MP1

Channel

Document

Movie

Photo

Report

Static

26-VOL-9999-MP1.mme

1

1.1.2 FW sub-test folders

• MAIN FOLDER NAME

...

Frontal FW test number

Channel

Document

Movie

Photo

Report

Static

MME-file

L ...

• 26-VOL-9999-Volvo XC90

1.

▶ 26-VOL-9999-FW1

Channel

Document

Movie

Photo

Report

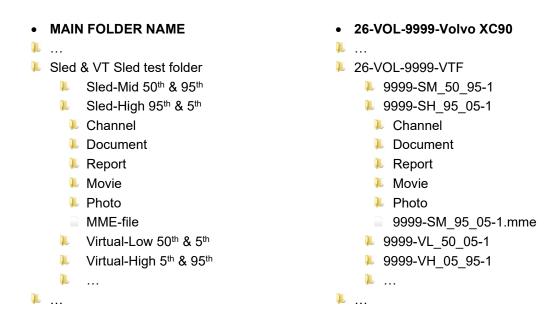
Static

26-VOL-9999-FW1.mme

L ...

1.1.3 Virtual Testing & Sled for Frontal sub-test folders

The Frontal VT & Sled test data folder contains eight sub-test folders, two for sled tests and six for virtual tests. This is data provided to Euro NCAP by the OEM. Note: In accordance with the VTC protocol, Euro NCAP will assign a unique test number that must be visible in the physical far side sled tests, XXX in the example below.



1.1.4 Side MDB sub-test folders

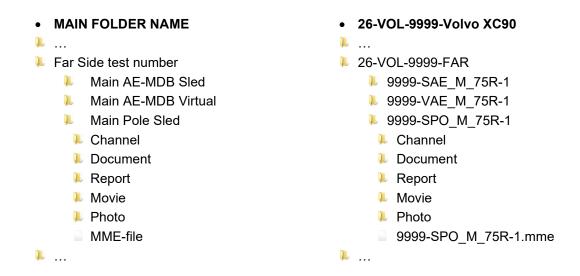


1.1.5 Side Pole sub-test folders



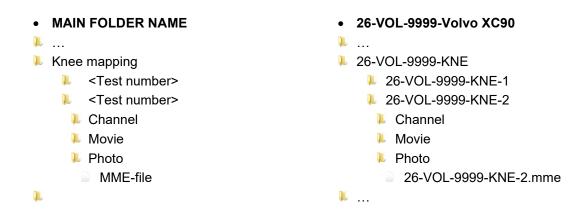
1.1.6 Far side sub-test folders

The Far side sled test data folder contains ten sub-test folders. This is data provided to Euro NCAP by the OEM. Note: In accordance with the VTC protocol, Euro NCAP will assign a unique test number that must be visible in the physical far side sled tests, XXX in the example below.



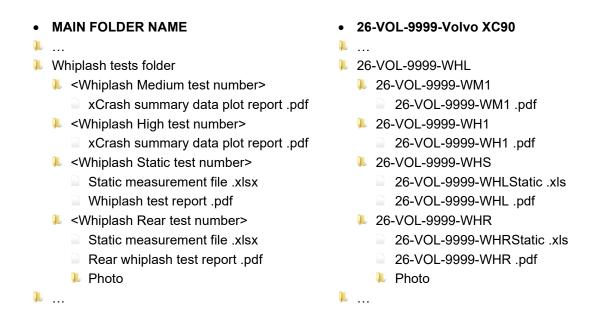
1.1.7 Knee mapping sub-test folders

The Knee mapping test folder contains a number of sub-test folders, one for each knee mapping test. This is data provided to Euro NCAP by the OEM.



1.1.8 Whiplash sub-test folders

The Whiplash test folder contains 4 sub-test folders. Two contain the dynamic data from the two dynamic pulses tested; Medium and High. In addition, the static whiplash data is contained in a separate folder, which also contains the static measurement file. The whiplash test report and the summary data plot report will be filed in the main Whiplash folder.



1.1.9 COP sub-test folders

The COP test folder contains 3 sub-test folders. They contain pictures and documents from both vehicle based assessment and the CRS installation checks as well as the vehicle manual (COP section). The COP test report will be filed in the main COP folder.

Euro NCAP

• MAIN FOLDER NAME

- L ...
- COP tests folder
 - CRS installation
 - Vehicle based assessment
 - Manual CRS vehicle lists
 - COP test report .pdf
- **L** ...

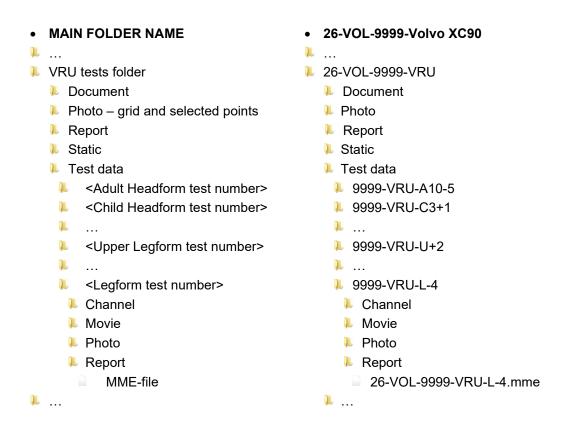
- 26-VOL-9999-Volvo XC90
- L ...
- ▶ 26-VOL-9999-COP
 - CRS installation
 - Vehicle based assessment
 - Manual-CRS vehicle lists
 - □ 26-VOL-9999-COP .pdf
- 1 ...

1.1.10 Vulnerable road user sub-test folders

The Vulnerable Road User test folder contains five sub-test folders. The document, photo, report and static folders containing general files from all tests including certification documents, test temperatures and grid/test point 3D measurements. The folder test data contains a folder for every tested point. For each of these tests there will be a separate sub-test folder (e.g. A10-5 folder), which needs to contain the channel and picture folders and the MME-file. The movie folder is needed where filming has been performed as defined in the film and photo protocol.

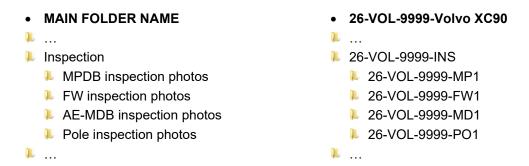
The test numbers for each sub-test consists of the Euro NCAP test number followed by the GRID point label.

The test report and the summary data plot report should be in the main report folder where the summary data plot report should contain all plots of all tests combined in one file called (20-VOL-9999-VRU.pdf).



1.1.11 Inspection folder structure

The Inspection test folder contains one sub-test folder for each crash test.



1.2 ISO MME folder structure

The ISO MME folder structure is to be applied to all applicable tests and the files contained in these folders follow the ISO/TS 13499 standard. The main directory contains six folders and two files. The following folders and files (comment files when needed) need to be provided for every test performed, where the test number is the one as specified in the previous section.

For each file and folder (where necessary) the required contents are specified in detail in the paragraphs below.

TEST NUMBER

- Channel
- Document
- Movie
- Photo
- Report
- Static
- <test number>.mme
- <test number>.txt

1.2.1 Channel folder

The channel folder contains all channels from the vehicle, impactors and dummies used in the test as defined in Section 2.

TEST NUMBER

- Channel
 - <test number>.xxx
- <test number>.chn
- 1

1.2.2 Document folder

The document folder contains the calibration documents and temperature log files for the test dummies used in the test.

TEST NUMBER

- **L** ...
- Document
 - < test number name of document file 1>
- < test number _ name of document file d>
- 1

1.2.3 Movie folder

The movie folder contains the inspection quality films, using the exact names as specified in the Euro NCAP Film and Photo protocol.

TEST NUMBER

- 1
- Movie
 - < test number _ name of movie file 1>
- < test number name of movie file m>
- 1

1.2.4 Photo folder

The photo folder contains the inspection quality photos in two folders "Before" and "After", where the name of the photo file consists of the test number followed by a number as specified in the Euro NCAP Film and Photo protocol.

TEST NUMBER

- **L** ...
- Photo
- Before
- < test number _ name of photo file 1>
- < test number name of photo file p>
- After
- < test number _ name of photo file 1>
- < test number _ name of photo file p>
- 1

1.2.5 Report folder

The report folder contains the test report containing the assessment data as described in the different test protocols and the data plots.

TEST NUMBER

- L ...
- Report
 - < test number name of test report>
 - < test number name of data plots>
 - < test number Belt buckle force report>
 - < test number _ Door opening force report>
 - < test number _ High voltage report>
- **L** ...

1.2.6 Static folder

The static folder contains the static measurements file where applicable containing the data as described in the different test protocols. In the MPDB test, this folder shall also contain the data required for the compatibility assessment and details of barrier reconstruction where applicable. Please note, the raw data file of the MPDB face scan is not required. In AE-MDB and pole impacts, this folder shall contain the post test door intrusion measurements. Where applicable, HPD and HCz reports shall be provided in the static folder for the relevant side or pole impact test.

TEST NUMBER

- Frontal MPDB test number
 - Static
- < test number name of static measurement file>
- < test number _ Compatibility assessment .xlsx>
- ...
- Side MDB and Side Pole test number
 - Static
 - < test number Door intrusion measurements file
 - < test number _ HPD report file> (pole test only)
 - < test number _ HCz report file> (pole test only)
- ...

1.2.7 MME-file

The mme-file contains the information of the test where the type of test and subtype of test shall be selected from the table below.

• TEST NUMBER



• <test number>.mme

The mme-file shall contain at least the following header:

Item	Header	Remarks
Data format edition number	:1.6	
Laboratory name	: <lab name=""></lab>	
Customer name	:Euro NCAP	
Customer test ref. number	: <test number=""></test>	See 0
Customer project ref. number	: <test number="" series=""></test>	4 digits number, e.g. 9999
Title	:Euro NCAP <rating year=""></rating>	Rating year, e.g. 2026
Timestamp	: <date> <time></time></date>	Date and time of MME file
Type of the test	: <see table=""></see>	See 0
Subtype of the test	: <see table=""></see>	See 0
Date of the test	: <date></date>	Date of test
Name of test object 1	: <make and="" model=""></make>	Make and Model exactly as per Euro NCAP DashBoard
Ref. number of test object 1	: <vin></vin>	
Velocity test object 1	: <vut speed=""></vut>	Actual test velocity of VUT
Mass test object 1	: <vut mass=""></vut>	Test mass of the VUT
Driver position object 1	:<1/3>	LHD=1, RHD=3
Impact side test object 1	: <le,ri></le,ri>	
Name of test object 2	: <name of="" target="" the=""></name>	See xxx
Velocity test object 2	: <target velocity=""></target>	Actual test velocity of target
Type of data source	: <type></type>	Simulation or Hardware

Additional mandatory lines when the "Type of data source" is Simulation:

Item	Header	Remarks
.Dummy Simulation Model Driver	: <dummy model="" simulation="" type=""> <name> <version> (<supplier>)</supplier></version></name></dummy>	e.g. HIII vxx (Humanetics)
.Dummy Qualification Ref Driver	: <name of="" pdf="">.pdf</name>	Reference to Document name e.g. xxx.pdf
.Dummy Simulation Model Passenger	: <dummy model="" simulation="" type=""> <name> <version> (<supplier>)</supplier></version></name></dummy>	e.g. HIII vxx (Humanetics)
.Dummy Qualification Ref Passenger	: <name of="" pdf="">.pdf</name>	Reference to Document name e.g. xxx.pdf
.Solver Name	: <fe name="" software=""></fe>	e.g. LS-Dyna
.Solver Version	: <fe software="" solver="" version=""></fe>	e.g. ls- dyna_mpp_s_R9_3_1_x64_ centos65_ifort131_sse2_openm pi183
.Solver Precision	: <solver precision=""></solver>	SP or DP
.Platform Name	: <name been="" have="" of="" on="" platform="" run="" simulations="" which=""></name>	e.g. centos78_openmpi2.1.3
.Number of CPUs	: <cores cpus="" x=""></cores>	e.g. 2x32
.Time step setting	: <min. in="" seconds="" size="" step="" time=""></min.>	e.g. min. time step 1-e7 s
.Contact Type dummy -seat	: <contact documentation="" type=""></contact>	e.g. S2S SOFT2 nu=0.2
.Contact Type dummy -belt	: <contact documentation=""></contact>	e.g. S2S SOFT2 nu=0.
.Contact Type dummy -airbag	: <contact documentation=""></contact>	e.g. S2S SOFT2 nu=0.
.Number of contacts	: <total contacts="" number="" of=""></total>	Number of contacts used in the overall simulation setup e.g. 10
.Number of elements	: <total elements="" number="" of=""></total>	e.g. 20000
.Mass of total setup in kg	: <total in="" kg="" mass=""></total>	Fill in in kg e.g. 1500 (used for quality checks)
.Mass of dummy 1 in kg	: <total in="" kg="" mass=""></total>	e.g. 75 (used for quality checks) - mass of driver dummy
.Mass of dummy 2 in kg	: <total in="" kg="" mass=""></total>	e.g. 75 (used for quality checks) - mass of passenger dummy
.Mass of seats in kg	: <total in="" kg="" mass=""></total>	e.g. 50 (used for quality checks)

Note: the non-standard attributes need to be preceded by a point ".xxx"

1.2.7.1 Customer test ref. number

Element	Sub-element	Loadcase	Customer test ref. number
Frontal Impact	Offset	MPDB-50	26-VOL-9999-MP?
	Full Width	FWDB-50	26-VOL-9999-FW?
	Sled & VT	Sled-Mid	9999-SM_50_95
		Sled-High	9999-SH_95_05
		Virtual-Low	9999-VL_50_05
			9999-VL_05_50
		Virtual-Mid	9999-VM_50_95
			9999-VM_50HBM
		Virtual-High	9999-VH_95_05
			9999-VH_05_95
Side Impact	MDB	AEMDB-50	26-VOL-9999-MD
	Pole	Pole-32	26-VOL-9999-PO
	Farside	Main-AEMDB	9999-SAE_M_75R
			9999-VAE_M_75R
		Main-Pole	9999-SPO_M_75R
			9999-VPO_M_75R
		Robustness-AEMDB	9999-VAE_R_60R
			9999-VAE_R_75H
			9999-VPO_R_90R
			9999-VPO_R_90H
		Robustness-Pole	9999-VPO_R_75H
			9999-VPO_R_90R
Rear Impact	Whiplash	Rear-Mid	26-VOL-9999-WM
		Rear-High	26-VOL-9999-WH
VRU Impact	Head impact	Headform	26-VOL-9999-HF
	Pelvis & Leg impact	Upper Legform	26-VOL-9999-UL
		Legform	26-VOL-9999-LF

1.2.7.2 Type and Subtype of test

The type and subtype of tests is summarised below:

Euro NCAP test	Type of Test	Subtype of test
Frontal Offset	Frontal Impact	MPDB-50
Frontal FW	Frontal Impact	FWDB-35
Frontal Sled & VT	Frontal Impact	Virtual-Low Sled-Mid Virtual-Mid Sled-High Virtual-High
Side MDB	Side Impact	AEMDB-50
Side Pole	Side Impact	Pole-32
Side Farside	Side Impact	Main-AEMDB Main-Pole Robustness-AEMDB60 Robustness-AEMDB75high Robustness-AEMDB90 Robustness-AEMDB90high Robustness-Pole75high Robustness-Pole90
Rear Whiplash	Rear Impact	Rear-Mid Rear-High
VRU	VRU Impact	Headform Upper Legform Legform

1.2.7.3 Name of test object 2

Element	Sub-element	Name of test object 2
Frontal Impact	Offset	MPDB
	Full Width	FWDB
	Sled & VT	-
Side Impact	MDB	AE-MDB
	Pole	Pole
	Farside	-
Rear Impact	Whiplash	-
VRU Impact	Head impact	Adult Headform Child Headform
	Pelvis Leg impact	Upper Legform aPLI

1.2.8 Txt file

The text file contains details of any test artefacts, errors or warnings associated with the test and how they should be considered.

- TEST NUMBER
 - **L** ...
 - <test number>.txt

2 CHANNEL NAMES AND FILTERS

For each dummy, impactors and test objects used in the different Euro NCAP tests, both physical and virtual, the following channel names shall be used. All channels shall be supplied either unfiltered or prefiltered. The appropriate filters for calculation of injury criteria and plotting of these channels will be performed by the analysis software used.

2.1 **Hybrid III 50%**

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000H3AC[X,Y,Z]P	1000
Neck	Forces, F _x F _y F _z	??NECKUP00H3FO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00H3MO[X,Y,Z]P	600
Chest	Accelerations, A _x A _y A _z	??CHST0000H3AC[X,Y,Z]P	180
	Deflection, D _{chest}	??CHST0003H3DSXP	180
Pelvis	Accelerations, A _x A _y A _z	??PELV0000H3AC[X,Y,Z]P	600
Lumbar Spine	Forces, F _x F _z	??LUSP0000H3FO[X,Z]P	600
	Moments, M _y	??LUSP0000H3MOYP	600
Femurs	Forces, F _z	??FEMR[LE,RI]00H3FOZP	600
Knees	Displacements, D _{knee}	??KNSL[LE,RI]00H3DSXP	180
Upper Tibia	Forces, F _x F _z	??TIBI[LE,RI]UPH3FO[X,Z]P	600
	Moments, M _x M _y	??TIBI[LE,RI]UPH3MO[X,Y]P	600
Lower Tibia	Forces, F _x F _z (F _y)	??TIBI[LE,RI]LOH3FO[X,Y,Z]P	600
	Moments, M _x M _y	??TIBI[LE,RI]LOH3MO[X,Y]P	600

Location	Parameter	ISO code	CFC
Head	Global Coordinates x,y,z	??HEAD0000H3DC[X,Y,Z]P	-
Chest	Global Coordinates x,y,z	??CHST0000H3DC[X,Y,Z]P	-
Pelvis	Global Coordinates x,y,z	??PELV0000H3DC[X,Y,Z]P	-
Complete dummy	Kinetic Energy	??EKINSU00H3EN00	-
	Internal Energy	??EINTSU00H3EN00	-
	Hourglass Energy	??EHOUSU00H3EN00	-
	Added Mass (absolute)	??MINCSU00H3MA00	-

2.2 THOR 50%

Location	Parameter	ISO code	CFC
Head	Acceleration, A _x A _y A _z	??HEAD0000T3AC[X,Y,Z]P	1000
	Angular rate sensor	??HEAD0000T3AV[X,Y,Z]P	60
	Tilt sensor, X Y	??HEADPR00T3AN[X,Y]P	-
Neck cable	Force, F _z	??NECK[FR,RE]00T3FOZP	1000
Upper Neck	Forces, F _x F _y F _z	??NECKUP00T3FO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00T3MO[X,Y,Z]P	600
T1	Acceleration, A _x A _y A _z	??THSP0100T3AC[X,Y,Z]P	600
T4	Acceleration, A _x A _y A _z	??THSP0400T3AC[X,Y,Z]P	600
Clavicle	Force, F _x F _z (Inner & Outer)	??CLAVLE[IN,OU]T3FO[X,Z]P	600
Thorax	Distance, DC0	??CHST[LE,RI][UP,LO]T3DC0P	180
	Angle, Y Z	??CHST[LE,RI][UP,LO]T3AN[Y,Z]P	180
Mid Sternum	Acceleration, A _x	??STRN0000T3ACXP	600
Abdomen	Distance, DC0	??ABDO[LE,RI]00T3DC0P	180
	Angle, Y Z	??ABDO[LE,RI]00T3AN[Y,Z]P	180
	Acceleration, A _x	??ABDO0000T3AC[X,Y,Z]P	600
T12	Acceleration, A _x A _y A _z	??THSP1200T3AC[X,Y,Z]P	180
	Force, F _x F _y F _z	??LUSP0000T3FO[X,Y,Z]P	600
	Moment, M _x M _y	??LUSP0000T3MO[X,Y]P	600
Pelvis	Acceleration, A _x A _y A _z	??PELV0000T3AC[X,Y,Z]P	600
	Tilt sensor, X Y	??PELVPR00T3AN[X,Y]P	-
ASIS	Force, F _x ,	??ILAC[LE,RI]00T3FOXP	600
	Moment, M _y	??ILAC[LE,RI]00T3MOYP	600
Acetabulum	Force, F _x F _y F _z	??ACTB[LE,RI]00T3FO[X,Y,Z]P	600
	Moment, My	??ILAC[LE,RI]00T3MOYP	600
Femurs	Force, F _x F _y F _z	??FEMR[LE,RI]00T3FO[X,Y,Z]P	600
	Moment, M _x M _y M _z	??FEMR[LE,RI]00T3MO[X,Y,Z]P	
Knees	Displacement, D _{knee}	??KNSL[LE,RI]00T3DSXP	180
Upper Tibia	Force, F _x F _z	??TIBI[LE,RI]UPT3FO[X,Z]P	600
Upper Tibia	Moment, M _x M _y	??TIBI[LE,RI]UPT3MO[X,Y]P	600
Lower Tibia	Force, F _x F _z	??TIBI[LE,RI]LOT3FO[X,Y,Z]P	600
	Moment, M _x M _y	??TIBI[LE,RI]LOT3MO[X,Y]P	600

2.3 Hybrid III 5%

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000HFAC[X,Y,Z]P	1000
Neck	Forces, F _x F _y F _z	??NECKUP00HFFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00HFMO[X,Y,Z]P	600
Chest	Accelerations, A _x A _y A _z	??CHST0000HFAC[X,Y,Z]P	180
	Deflection, D _{chest}	??CHST0003HFDSXP	180
Pelvis	Accelerations, A _x A _y A _z	??PELV0000HFAC[X,Y,Z]P	600
Iliac	Forces, F _x	??ILAC[LE,RI]00HFFOXP	600
	Moments, M _y	??ILAC[LE,RI]00HFMOYP	600
Lumbar Spine	Forces, F _x F _z	??LUSP0000HFFO[X,Z]P	600
	Moments, M _y	??LUSP0000HFMOYP	600
Femurs	Forces, F _z	??FEMR[LE,RI]00HFFOZP	600
Knees	Displacements, D _{knee}	??KNSL[LE,RI]00HFDSXP	180
Upper Tibia	Forces, F _x F _z	??TIBI[LE,RI]UPHFFO[X,Z]P	600
	Moments, M _x M _y	??TIBI[LE,RI]UPHFMO[X,Y,Z]P	600
Lower Tibia	Forces, F _x F _z (F _y)	??TIBI[LE,RI]LOHFFO[X,Y,Z]P	600
	Moments, M _x M _y	??TIBI[LE,RI]LOHFMO[X,Y,Z]P	600

Location	Parameter	ISO code	CFC
Head	Global Coordinates x,y,z	??HEAD0000HFDC[X,Y,Z]P	-
Chest	Global Coordinates x,y,z	??CHST0000HFDC[X,Y,Z]P	-
Pelvis	Global Coordinates x,y,z	??PELV0000HFDC[X,Y,Z]P	-
Complete dummy	Kinetic Energy	??EKINSU00HFEN00	-
	Internal Energy	??EINTSU00HFEN00	-
	Hourglass Energy	??EHOUSU00HFEN00	-
	Added Mass (absolute)	??MINCSU00HFMA00	-

2.4 Hybrid III 95%

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000HMAC[X,Y,Z]P	1000
Neck	Forces, F _x F _y F _z	??NECKUP00HMF0[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00HMMO[X,Y,Z]P	600
Chest	Accelerations, A _x A _y A _z	??CHST0000HMAC[X,Y,Z]P	180
	Deflection, D _{chest}	??CHST0003HMDSXP	180
Pelvis	Accelerations, A _x A _y A _z	??PELV0000HMAC[X,Y,Z]P	600
Lumbar Spine	Forces, F _x F _z	??LUSP0000HMFO[X,Z]P	600
	Moments, M _y	??LUSP0000HMMOYP	600
Femurs	Forces, Fz	??FEMR[LE,RI]00HMFOZP	600
Knees	Displacements, D _{knee}	??KNSL[LE,RI]00HMDSXP	180
Upper Tibia	Forces, F _x F _z	??TIBI[LE,RI]UPHMFO[X,Z]P	600
	Moments, M _x M _y	??TIBI[LE,RI]UPHMMO[X,Y]P	600
Lower Tibia	Forces, F _x F _z (F _y)	??TIBI[LE,RI]LOHMFO[X,Y,Z]P	600
	Moments, M _x M _y	??TIBI[LE,RI]LOHMMO[X,Y]P	600

Location	Parameter	ISO code	CFC
Head	Global Coordinates x,y,z	??HEAD0000HMDC[X,Y,Z]P	-
Chest	Global Coordinates x,y,z	??CHST0000HMDC[X,Y,Z]P	-
Pelvis	Global Coordinates x,y,z	??PELV0000HMDC[X,Y,Z]P	-
Complete dummy	Kinetic Energy	??EKINSU00HMEN00	-
	Internal Energy	??EINTSU00HMEN00	-
	Hourglass Energy	??EHOUSU00HMEN00	-
	Added Mass (absolute)	??MINCSU00HMMA00	-

2.5 WorldSID 50%

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000WSAC[X,Y,Z]P	1000
	Angular rate sensor	??HEAD0000WSAV[X,Y,Z]P	60
Upper Neck	Forces, F _x F _y F _z	??NECKUP00WSFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00WSMO[X,Y,Z]P	600
Lower Neck	Forces, F _x F _y F _z	??NECKLO00WSFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKLO00WSMO[X,Y,Z]P	600
Shoulder	Forces, Fx, Fy, Fz	??SHLD[LE,RI]00WSFO[X,Y,Z]P	600
	Distance, R	??SHRI[LE,RI]00WSDC0P	180
	Rotation, α	??SHRI[LE,RI]00WSANZP	180
Thorax	Distance, R	??TRRI[LE,RI][01,02,03]WSDC0P	180
	Rotation, α	??TRRI[LE,RI][01,02,03]WSANZP	180
T4	Accelerations, A _x A _y A _z	??THSP0400WSAC[X,Y,Z]P	180
Abdomen	Distance, R	??ABRI[LE,RI][01,02]WSDC0P	180
	Rotation, α	??ABRI[LE,RI][01,02]WSANZP	180
T12	Accelerations, A _x A _y A _z	??THSP1200WSAC[X,Y,Z]P	180
Lumbar Spine	Forces, F _x F _y F _z	??LUSP0000WSFO[X,Y,Z]P	600
	Moments, M _x M _y M _z	??LUSP0000WSMO[X,Y,Z]P	600
Pelvis	Accelerations, A _x A _y A _z	??PELV0000WSAC[X,Y,Z]P	600
	Forces, F _y	??PUBC0000WSFOYP	600
Femoral Neck	Forces, F _x F _y F _z	??FEAC[LE,RI]00WSFO[X,Y,Z]P	600

Location	Parameter	ISO code	CFC
Head	Global Coordinates x,y,z	??HEAD0000WSDC[X,Y,Z]P	-
T4	Global Coordinates x,y,z	??THSP0400WSDC[X,Y,Z]P	-
T12	Global Coordinates x,y,z	??THSP1200WSDC[X,Y,Z]P	
Pelvis	Global Coordinates x,y,z	??PELV0000WSDC[X,Y,Z]P	-
Complete dummy	Kinetic Energy	??EKINSU00WSEN00	-
	Internal Energy	??EINTSU00WSEN00	-
	Hourglass Energy	??EHOUSU00WSEN00	-
	Added Mass (absolute)	??MINCSU00WSMA00	-

2.6 BioRID UN

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000BRAC[X,Y,Z]P	60
	Velocity, V _x	??HEAD0000BRVEXV	30
	Contact	??HERE000000EV00	-
Cervical Spine	Accelerations, A _x A _z	??CESP0400BRAC[X,Z]P	60
Neck Upper	Forces, F _x F _y F _z	??NECKUP00BRFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00BRMO[X,Y,Z]P	600
Neck Lower	Forces, F _x F _y F _z	??NECKLO00BRFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKLO00BRMO[X,Y,Z]P	600
T1	Accelerations, A _x A _z	??THSP01[LE,RI]BRAC[X,Z]P	60
Т8	Accelerations, A _x A _z	??THSP0800BRAC[X,Z]P	60
Lumbar Spine	Accelerations, A _x A _z	??LUSP0100BRAC[X,Z]P	60
Pelvis	Accelerations, A _x A _y A _z	??PELV0000BRAC[X,Y,Z]P	60

2.7 Q6

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000Q6AC[X,Y,Z]P	1000
Neck Upper	Forces, F _x F _y F _z	??NECKUP00Q6FO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00Q6MO[X,Y,Z]P	600
Thorax	Accelerations, A _x A _y A _z	??THSP0000Q6AC[X,Y,Z]P	180
	Displacement, D	??CHST0000Q6DSXP	180

2.8 Q10

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	??HEAD0000QBAC[X,Y,Z]P	1000
Neck Upper	Forces, F _x F _y F _z	??NECKUP00QBFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??NECKUP00QBMO[X,Y,Z]P	600
Shoulder (side only)	Accelerations, A _x A _y A _z	??THSP0000Q6AC[X,Y,Z]P	180
T1 (side only)	Displacement, D	??CHST0000Q6DSXP	180
T4	Accelerations, A _x A _y A _z	??THSP0400QBAC[X,Y,Z]P	180
Chest (frontal only)	Distance, R	??CHST[LO,UP]00QBDC0P	180
	Rotation, α	??CHST[LO,UP]00QBANZP	180
Chest (side only)	Distance, R	??CHST[LE,RI][LO,UP]QBDC0P	180
	Rotation, α	??CHST[LE,RI][LO,UP]QBANZP	180
Lumbar Spine	Forces, F _x F _y F _z	??LUSP0000QBFO[X,Y,Z]P	1000
	Moments, M _x M _y M _z	??LUSP0000QBMO[X,Y,Z]P	600
Pelvis-Sacrum	Accelerations, A _x A _y A _z	??PELV0000QBAC[X,Y,Z]P	180
Pelvis-Pubis (side only)	Forces, Fy	??PUBC0000QBFOYP	1000

2.9 Adult headform

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	D0HEAD0000PJAC[X,Y,Z]P	1000

2.10 Small adult / child headform

Location	Parameter	ISO code	CFC
Head	Accelerations, A _x A _y A _z	D0HEAD0000PSAC[X,Y,Z]P	1000

2.11 Upper legform

Location	Parameter	ISO code	CFC
Femur	Forces, F _x	D0FEMR[UP,LO]00PUFOXP	180
	Moments, M _y	D0FEMR[UP,MI,LO]00PUMOYP	180

2.12 Legform (aPLI)

Location	Parameter	ISO code	CFC
Upper Mass	Accelerations, A _x A _y A _z	??PELV0000PMAC[X,Y,Z]P	180
	Angular velocity	??PELV0000PMAV[X,Y]P	180
Femur	Moments, M _x	??FEMR[UP,MI,LO]00PMMOXP	180
Knee	Displacement, D _{MCL}	??KNEEMC00PMDS0P	180
	Displacement, D _{PCL}	??KNEEPC00PMDS0P	180
	Displacement, D _{ACL}	??KNEEAC00PMDS0P	180
Tibia	Moments, M _x	??TIBI[UP,LO]00PMMOXP	180
		??TIBIMI[UP,LO]PMMOXP	180

2.13 Vehicle

Location	Parameter	ISO code	CFC
B-Pillar	Accelerations, A _x A _y	[14,16]BPILL00000AC[X,Y]P	60
Seatbelt, B3	Force, F _{seatbelt}	??SEBE0003B3F00P	60
Seatbelt, B6	Force, F _{seatbelt}	??SEBE0003B6FO0P	60
Vehicle trunk	Angular rate sensor	18TUNN000000AV[X,Y,Z]P	60

2.14 Trolley

Location	Parameter	ISO code	CFC
CoG	Accelerations, A _x	M0MBARCG0000ACXP	60
			180

2.15 Sled

Location	Parameter	ISO code	CFC
Sled	Accelerations, A _x	S0SLED000000ACXP	60

Location	Parameter	ISO code	CFC
Seat	Kinetic Energy	??EKINSU0000EN00	-
	Internal Energy	??EINTSU0000EN00	-
	Hourglass Energy	??EHOUSU0000EN00	-
	Added Mass (absolute)	??MINCSU0000MA00	-

2.16 Virtual Tests

Location	Parameter	ISO code	CFC
Contact Dummy – Seat	Force, F_x , F_y , F_z	??SEAT0000??FO[X,Y,Z]P	-
Contact Dummy – Seatbelt	Force F _x , F _y , F _z	??SEBE0000??FO[X,Y,Z]P	-
Global	Global Kinetic Energy	00EKINSU0000EN00	-
Global	Global Internal Energy	00EINTSU0000EN00	-
Global	Global Hourglass Energy	00EHOUSU0000EN00	-
Global	Global External Work	00EXWOSU0000EN00	-
Global	Added Mass (absolute)	00MINCSU00000000	-
Global	Total Energy	00ETOTSU0000EN00	-

3 INJURY CRITERIA CALCULATION

This chapter describes the calculation for each injury criterion including the filters that are applied to each channel used in these calculations. The analysis software used by the Euro NCAP labs will follow these calculations in detail.

For all of the calculations and for all of the dummies used, only the loading phase of the crash is considered. Usually, the loading phase for all dummies in the frontal tests will end at the point in time where the filtered head acceleration A_x crosses zero g after the minimum acceleration peak value. This does not apply to the farside occupant-to-occupant test, the loading phase to evaluate occupant-to-occupant interaction will end when all parts of both dummies are moving outboard.

It is up to Euro NCAP to confirm and determine the actual end of the loading phase.

3.1 Head criteria

3.1.1 Head resultant acceleration

The head resultant acceleration is calculated with the following formula:

$$A_R = \sqrt{{A_x}^2 + {A_y}^2 + {A_z}^2}$$

with:

 $\begin{array}{lll} A_x & & \text{Filtered Head Acceleration A}_x & & ??\text{HEAD0000??ACXA} \\ A_y & & \text{Filtered Head Acceleration A}_y & & ??\text{HEAD0000??ACXA} \\ A_z & & \text{Filtered Head Acceleration A}_z & & ??\text{HEAD0000??ACZA} \end{array}$

3.1.2 HIC₁₅

The HIC₁₅ value is calculated with the following formula:

$$HIC_{15} = (t_2 - t_1) \left(\frac{1}{(t_2 - t_1)} \int_{t_1}^{t_2} A_R dt \right)^{2.5}$$

with:

A_R Head Resultant Acceleration

3.1.3 Diffuse axonal multi-axis general evaluation (DAMAGE)

The DAMAGE criterion is calculated with the following formulae over the time window specified below. Head rotational velocity, filtered at CFC 60, shall be used to generate rotational acceleration throughout the impact.

$$\begin{bmatrix} m_x & 0 & 0 \\ 0 & m_y & 0 \\ 0 & 0 & m_z \end{bmatrix} \begin{pmatrix} \ddot{\delta}_x \\ \ddot{\delta}_y \\ \ddot{\delta}_z \end{pmatrix} + \begin{bmatrix} c_{xx} + c_{xy} + c_{xz} & -c_{xy} & -c_{xz} \\ -c_{xy} & c_{xy} + c_{yy} + c_{yz} & -c_{yz} \\ -c_{xz} & -c_{yz} & c_{xz} + c_{yz} + c_{zz} \end{bmatrix} \begin{pmatrix} \dot{\delta}_x \\ \dot{\delta}_y \\ \dot{\delta}_z \end{pmatrix} + \begin{bmatrix} k_{xx} + k_{xy} + k_{xz} & -k_{xy} & -k_{xz} \\ -k_{xy} & k_{xy} + k_{yy} + k_{yz} & -k_{yz} \\ -k_{xz} & -k_{yz} & k_{xz} + k_{yz} + k_{zz} \end{bmatrix} \begin{pmatrix} \delta_x \\ \delta_y \\ \delta_z \end{pmatrix} = \begin{bmatrix} m_x & 0 & 0 \\ 0 & m_y & 0 \\ 0 & 0 & m_z \end{bmatrix} \begin{pmatrix} \ddot{u}_x \\ \ddot{u}_y \\ \ddot{u}_z \end{pmatrix}$$

$$DAMAGE = \beta max_t \{ |\vec{\delta}(t)| \}$$
$$\vec{\delta}(t) = [\delta_x(t) \quad \delta_y(t) \quad \delta_z(t)]^T, \ \beta = \text{scale factor}$$

 $m = mass, c_{ij} = damping, k_{ij} = stiffness$

 $\ddot{\delta}, \dot{\delta}, \delta = acceleration, velocity, displacement$

 $\ddot{u} = applied \ angular \ acceleration$

$$m_x = 1 kg, m_y = 1 kg, m_z = 1 kg$$

$$k_{xx} = 32142 \, N/m, k_{yy} = 23493 \, N/m, k_{zz} = 16935 \, N/m,$$

$$k_{xy} = 0 N/m, k_{yz} = 0 N/m, k_{xz} = 1636.3 N/m, a1=5.9148 ms, \beta=2.9903 1/m$$

$$[c] = a1 \times [k]$$

When calculating DAMAGE, a time window is specified to exclude certain secondary contacts between the head and vehicle interior. Note, this window does not apply to either HIC or 3ms exceedance calculations. The exclusion criteria are based upon those used by JNCAP.

This criterion will be evaluated during the loading and early rebound phases of the impact over a max period from T0 up to 200ms. The time window will be reduced to less than 200ms if, during head rebound, a secondary impact results in an external force on the head drops below -500N.

The external force acting on the head shall be calculated using the head x acceleration and upper neck x force using the formula below. End the calculation when: F external x < -500N

$$F_{external\,x} = -M_{Head} \times a_{Head\,x} + F_{Neck_{upper}x}$$

Where $M_{Head} = 4.2 kg$.

3.1.4 Head restraint contact time

The head restraint contact time is calculated with the following formula:

 $T_{HRC} = T_{HRC,end} - T_{HRC,start}$ with:

 $T_{\text{HRC},\text{start}}$ Time of first contact of head and HR after T=0

??HERE000000EV00

T_{HRC.end} Time where contact is lost

??HERE000000EV00

Head restraint contact time $T_{HRC(Start)}$ is defined as the time (calculated from T=0) of first contact between the rear of the ATD head and the head restraint, where the subsequent continuous contact duration exceeds 40ms. For the purposes of assessment, $T_{HRC(Start)}$ shall be rounded to the nearest millisecond. Gaps up to 1ms are ignored if proven to be the result of poor electrical contact. $T_{HRC}_{(end)}$ is defined as the time at which the head first loses contact with the head restraint, where the subsequent continuous loss of contact duration exceeds 40ms.

3.1.5 Head rebound velocity

The head rebound velocity (in the horizontal/X direction) shall be determined using dummy head CoG target tracking from camera footage. Head rebound velocity shall be calculated as follows:

$$V_{Rebound} = V_{Head CoG (abs)} - V_{Sled (abs)}$$

Where:

 $V_{Rebound}$ = Instantaneous rebound X-velocity of the head c-of-g, relative to the sled

V _{Head CoG (abs)} = Instantaneous X-velocity of head centre of gravity, absolute.

 $V_{Sled (abs)}$ = Instantaneous X-velocity of sled, absolute.

3.1.6 T1 x-acceleration

The T1 x-acceleration value is calculated with the following formula:

 $T1 = \frac{T1_{left} + T1_{right}}{2}$

with:

T1_{left} Filtered left T1 acceleration ??THSP01LEBRACXD
T1_{right} Filtered right T1 acceleration ??THSP01RIBRACXD

The maximum, $T1_{max}$, should be generated from this average T1 channel, considering only the portion of data from T-zero until T-HRC_(end) as follows:

$$T1_{max} = \max_{T-HRC_{(end)}} [T1(t)]$$

3.2 Neck criteria

3.2.1 Neck extension bending moment @ OC

The neck extension bending moment is calculated with the following formula:

$$M_{OCy} = M_y - F_x \cdot d$$

with:

 M_y Filtered Bending Moment ??NECKUP00??MOYB F_x Filtered Shear Force ??NECKUP00??FOXB

d 0.01778m for all HIII series and 0.0195m for WorldSID

3.2.2 Neck lateral flexion bending moment @ OC

The neck lateral flexion bending moment is calculated with the following formula:

$$M_{OCx} = M_x + F_y \cdot d$$

with:

 M_x Filtered Bending Moment ??NECKUP00WSMOXB F_y Filtered Shear Force ??NECKUP00WSFOYB

d 0.0195m WorldSID

3.2.3 Neck extension bending moment

The neck extension bending moment is calculated with the following formula:

$$M_{\nu} = abs(\min(M_{\nu}))$$

with:

M_y Filtered Bending Moment for THOR ??NECKUP00??MOYB
M_y Filtered Bending Moment for WorldSID ??NECKLO00??MOYB

3.2.4 Neck lateral flexion bending moment @ Neck base

The neck lateral flexion bending moment is calculated with the following formula:

$$Mx_{(base\ of\ neck)} = \max(\ abs(Mx_M - Fy_m \times Dz))$$

with:

MxM = Filtered Bending Moment ??NECKLO00WSMOXB FyM = Filtered Shear Force ??NECKLO00WSFOYB

Dz = 0.0145m for WorldSID (ISO 15830)

$$My_{(base\ of\ neck)} = |\min(My_M + Fx_M * Dz)|$$

with:

MyM =Filtered Bending Moment??NECKLO00WSMOYBFxM =Filtered Shear Force??NECKLO00WSFOXB

Dz = 0.0145m for WorldSID (ISO 15830)

3.2.5 Upper and lower neck shear force and tension

Positive shear shall indicate head-rearwards motion and positive tension should be associated with pulling the head upwards, generating a tensile force in the neck. Firstly, the Fx and Fz channels shall be filtered as defined in Section 2.6. Peak values shall be determined for each of the forces, considering only the portion of data from T-zero until T-HRC(end), as follows:

$$Fx_{max} = \max_{T-HRC_{(end)}} [Fx(t)]$$

$$Fz_{max} = \underset{T-HRC_{(end)}}{\text{Max}} [Fz(t)]$$

3.2.6 NIC

The NIC value is calculated with the following formula:

$$NIC = 0.2 \cdot A_{rel} + v_{rel}^2$$

with:

$$A_{rel} = T1 - A_{x,head}$$

$$v_{rel} = \int A_{rel}$$

T1 Average T1 acceleration

A_{x,head} Filtered Head Acceleration A_x

??HEAD0000BRACXD

??NECKUP00BRFOXB

??NECKUP00BRMOYB

3.2.7 Nkm

The Nkm value is calculated with the following formula:

$$Nkm(t) = N_{ep}(t) + N_{ea}(t) + N_{fp}(t) + N_{fa}(t)$$
...

with:

$$N_{ep}(t) = \frac{M_{ocye}(t)}{-47.5Nm} + \frac{F_{xp}(t)}{-845N}$$

$$N_{ea}(t) = \frac{M_{ocye}(t)}{-47.5Nm} + \frac{F_{xa}(t)}{845N}$$

$$N_{fp}(t) = \frac{M_{ocyf}(t)}{88.1Nm} + \frac{F_{xp}(t)}{-845N}$$

$$N_{fa}(t) = \frac{M_{ocyf}(t)}{88.1Nm} + \frac{F_{xa}(t)}{845N}$$

$$M_{OCv}(t) = M_v(t) - D \cdot F_x(t)$$

 $F_x(t)$ Filtered Upper Neck Shear Force F_x

M_y(t) Filtered Upper Neck Moment M_y

D 0.01778m

 $F_{xp}(t)$ negative portion of $F_x(t)$

 $F_{xa}(t)$ positive portion of $F_x(t)$

 $M_{ye}(t)$ negative portion of $M_{OCy}(t)$

 $M_{vf}(t)$ positive portion of $M_{OCv}(t)$

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When the 4 criteria are calculated, particular forces and moments must be set to 0. This is an AND condition. That is if one of the summands is zero, the condition is also zero. Consider only the portion of data from T-zero until T-HRC(end).

3.3 Shoulder criteria

3.3.1 Lateral shoulder force

The Lateral Shoulder Force is calculated with the following formula:

$$Fy_{shoulder} = abs\left(\min\left(F_y(t)\right)\right)$$
 with:
 F_y Filtered Shoulder Force F_y ??SHLD[LE,RI]00WSFOYB

3.3.2 Lateral shoulder rib displacement

The lateral shoulder rib displacement is calculated with the following formula:

$$\begin{array}{ll} Dy_{shoulder} = \max \bigl(D_y(t) - D_y(0) \bigr) \\ \text{with:} \\ D_y(t) = R(t) \cdot \sin (\Phi(t)) \\ \text{R(t)} \qquad \text{Filtered Shoulder sensor length} \\ \qquad ?? \text{SHRI[LE,RI]00WSDC0C} \\ \Phi(t) \qquad \text{Filtered Shoulder sensor rotation} \qquad ?? \text{SHRI[LE,RI]00WSANZC} \\ D_y(0) \qquad \text{Lateral Shoulder Rib Displacement @ t=0} \end{array}$$

Further details regarding definitions for measurement coordinate system, sensor offsets and polarities, and post-processing can be found in ISO/TS21002.

3.4Chest criteria

3.4.1 Chest deflection

The chest deflection value is calculated with the following formula:

$$D_{chest} = \max (D_{chest}(t))$$
 with:

D_{chest}(t) Filtered Chest Deflection D_{chest}

??CHST0003??DSXC

3.4.2 Chest rib displacement

The chest rib displacement is calculated with the following formula:

$$D_{rib} = max \left(\sqrt{D_x(t)^2 + D_y(t)^2 + D_z(t)^2} \right)$$

with:

$$D_{x}(t) = \delta \cdot \sin(\Phi_{y}(t)) + R(t) \cdot \cos(\Phi_{z}(t)) \cdot \cos(\Phi_{y}(t)) - D_{x}(0)$$

$$D_{y}(t) = R(t) \cdot \sin(\Phi_{z}(t)) - D_{y}(0)$$

$$D_{z}(t) = \delta \cdot \cos(\Phi_{y}(t)) - R(t) \cdot \cos(\Phi_{z}(t)) \cdot \sin(\Phi_{y}(t)) - D_{z}(0)$$

R(t) Filtered Chest Rib sensor length ??CHST[LE,RI][UP,LO]T3DC0C $\Phi_y(t)$ Filtered Chest Rib sensor rotation ??CHST[LE,RI][UP,LO]T3ANYC $\Phi_z(t)$ Filtered Chest Rib sensor rotation ??CHST[LE,RI][UP,LO]T3ANZC $\Phi_{[x,y,z]}(0)$ Chest Rib Displacement in x,y,z direction @ t=0 +15.65mm for Upper Chest Rib and -15.65mm for Lower Chest Rib

Definitions regarding measurement coordinate system, sensor offsets and polarities, and post-processing can be found in ISO/TS21002. Where a vehicle is equipped with pretensioners that activate before T0, the displacement prior to activation shall be used for $D_{x,y,z}(0)$.

Rmax is used for the injury calculation.

3.4.3 Chest displacement

The Q10 chest displacement in the MPDB test is calculated for the upper and lower measurement system with the following formula:

$$D_{rib} = max \left(\sqrt{D_x(t)^2 + D_y(t)^2} \right)$$

with:

$$D_x(t) = R(t) \cdot cos(\Phi_z(t)) - D_x(0)$$

$$D_y(t) = R(t) \cdot sin(\Phi_z(t)) - D_y(0)$$

R(t) Filtered sensor length $\Phi_z(t)$ Filtered sensor rotation

??CHST[LO,UP]00QBDC0C ??CHST[LO,UP]00QBANZC

 $D_{[x,y]}(0)$ Chest Displacement @ t=0

Definitions regarding measurement coordinate system, sensor offsets and polarities, and post-processing can be found in ISO/TS21002. Where a vehicle is equipped with pretensioners that activate before T0, the displacement prior to activation shall be used for $D_{[x,y]}(0)$.

3.4.4 Seatbelt force

The Seatbelt force modifier is calculated with the following formula:

 $F_{seatbelt} = \max (F_{seatbelt}(t))$ with: $F_{seatbelt}$ Filtered Seatbelt Force

??SEBE0003B3FO0D

3.4.5 Lateral Thoracic Rib Displacement

The lateral thoracic rib displacement is calculated with the following formula:

 $\begin{array}{ll} Dy_{thorax} = \max \bigl(D_y(t) - D_y(0)\bigr) \\ \text{with:} \\ D_y(t) = R(t) \cdot \sin(\Phi(t)) \\ \text{R}(t) \qquad \text{Filtered Thoracic sensor length} \\ \Phi(t) \qquad \text{Filtered Thoracic sensor rotation} \\ D_y(0) \qquad \text{Lateral Thoracic Rib Displacement @ t=0} \end{array} \begin{array}{ll} ??TRRI[\text{LE,RI}]01??DC0C} \\ ??TRRI[\text{LE,RI}]01??ANZC \\ \end{array}$

Definitions regarding measurement coordinate system, sensor offsets and polarities, and post-processing can be found in ISO/TS21002.

3.4.6 Viscous Criterion

The VC is calculated with the following formula:

$$\begin{array}{ll} \textit{VC} = \textit{sf} \cdot \textit{V}(t) \times \textit{C}(t) \\ \textit{With:} \\ \textit{sf} & 1.3 \text{ for HIII-50, } 1.3 \text{ for HIII-05 and } 1.0 \text{ for WorldSID} \\ \textit{V}(t) = \frac{8(\textit{D}_{chest}(t+1) - \textit{D}_{chest}(t-1)) - (\textit{D}_{chest}(t+2) - \textit{D}_{chest}(t-2))}{12\Delta t} \\ \textit{C}(t) = \frac{\textit{D}_{chest}(t)}{\textit{D}_{constant}} \\ \textit{D}_{chest}(t) & \textit{Filtered Chest Deflection D}_{chest} & ??\textit{CHST0003??DSXC} \\ & \textit{for WorldSID use calculated Lateral Thoracic Rib Displacement Dy}_{thorax} \\ \Delta t & \textit{Time step} \\ \textit{D}_{constant} & 0.229 \text{ for HIII-50, } 0.187 \text{ for HIII-05 and } 0.170 \text{ for WorldSID [Q10 TBC]} \\ \end{array}$$

3.5 Abdominal criteria

3.5.1 T12 resultant acceleration

The T12 resultant acceleration is calculated with the following formula:

$$A_{R} = \sqrt{{A_{x}}^{2} + {A_{y}}^{2} + {A_{z}}^{2}}$$

with:

 $\begin{array}{lll} A_x & & \text{Filtered T12 Acceleration A}_x & & ??\text{THSP1200WSACXC} \\ A_y & & \text{Filtered T12 Acceleration A}_y & & ??\text{THSP1200WSACYC} \\ A_z & & \text{Filtered T12 Acceleration A}_z & & ??\text{THSP1200WSACZC} \end{array}$

3.5.2 Abdominal rib displacement (THOR)

The abdominal rib displacement is calculated with the following formula:

$$D_{rib} = max(D_x(t))$$

with:

$$D_x(t) = R(t) \cdot \cos(\Phi_z(t)) \cdot \cos(\Phi_v(t)) - D_x(0)$$

R(t)	Filtered Abdominal Rib sensor length	??ABDO[LE,RI]00T3DC0C	
$\Phi_{y}(t)$	Filtered Abdominal Rib sensor rotation	??ABDO[LE,RI]00T3ANYC	
$\Phi_z(t)$	Filtered Abdominal Rib sensor rotation	??ABDO[LE,RI]00T3ANZC	
$D_{[x,y,z]}(0)$	Abdominal Rib Displacement in x,y,z direction @ t=0		

Definitions regarding measurement coordinate system, sensor offsets and polarities, and post-processing can be found in ISO/TS21002. Where a vehicle is equipped with pretensioners that activate before T0, the displacement prior to activation shall be used for $D_{x,y,z}(0)$.

3.5.3 Lateral abdominal rib displacement

The lateral abdominal rib displacement is calculated with the following formula:

$$\begin{array}{ll} Dy_{abdomen} = \max \bigl(D_y(t) - D_y(0) \bigr) \\ \text{with:} \\ D_y(t) = R(t) \cdot \sin(\Phi(t)) \\ \text{R(t)} \qquad \text{Filtered Abdominal sensor length} \qquad ??\text{ABRI[LE,RI]01WSDC0C} \\ \Phi(t) \qquad \text{Filtered Abdominal sensor rotation} \qquad ??\text{ABRI[LE,RI]01WSANZC} \\ D_y(0) \qquad \text{Lateral Abdominal Rib Displacement @ t=0} \end{array}$$

Definitions regarding measurement coordinate system, sensor offsets and polarities, and post-processing can be found in ISO/TS21002.

3.5.4 Viscous criterion

The VC is calculated with the following formula:

$$\label{eq:VC} \begin{split} &VC = sf \cdot V(t) \times C(t) \\ &\text{With:} \\ &\text{sf} & 1.0 \text{ for WorldSID} \\ &V(t) = \frac{8(D_{y,abdomen}(t + \Delta t) - D_{y,abdomen}(t - \Delta t)) - (D_{y,abdomen}(t + 2\Delta t) - D_{y,abdomen}(t - 2\Delta t))}{12\Delta t} \\ &C(t) = \frac{D_{y,abdomen}(t)}{D_{constant}} \\ &\text{Dy}_{abdomen}(t) & \text{Calculated Lateral Abdominal Rib Displacement} \\ &\Delta t & \text{Time step} \\ &D_{constant} & 0.170 \text{ for WorldSID} \end{split}$$

3.6 Lower extremity criteria

3.6.1 Iliac force drop

The iliac force drop value is calculated with the following formula:

$$\begin{split} IFD &= \max{(IFD(t))} \\ \text{With:} \\ IFD(t) &= F_{iliac}(t+0.001s) - F_{iliac}(t) \\ F_{iliac} &\text{(t)} \quad \text{Filtered Iliac Force } F_{iliac} &\text{??ILAC[LE,RI]00??FOXB} \end{split}$$

3.6.2 Acetabulum force

The resultant acetabulum force value is calculated with the following formula for time intervals where $F_{\text{acetabulum},X}$ is in compressive load:

$$F_{acetabulum} = \max \left(\sqrt{F_{acetabulum,X}^2 + F_{acetabulum,Y}^2 + F_{acetabulum,Z}^2} \right)$$
 With:
$$F_{acetabulum,X} \qquad Filtered \ Femur \ Force \ F_{acetabulum,X} \qquad ??ACTB[LE,RI]00T3FOXB \\ F_{acetabulum,Y} \qquad Filtered \ Femur \ Force \ F_{acetabulum,Y} \qquad ??ACTB[LE,RI]00T3FOYB \\ F_{acetabulum,Z} \qquad Filtered \ Femur \ Force \ F_{acetabulum,Z} \qquad ??ACTB[LE,RI]00T3FOZB$$

3.6.3 Knee displacement

The knee displacement value is calculated with the following formula:

$$D_{knee} = |\min(D_{knee}(t))|$$

With:
 $D_{knee}(t)$ Filtered Knee Displacement D_{knee} ??KNSL[LE,RI]00??DSXC

3.6.4 Femur force

The femur force value is calculated with the following formula:

$$F_{femur} = abs \left(min \left(F_{femur}(t) \right) \right)$$

Filtered Femur Force F_{femur} F_{femur}(t)

??FEMR[LE,RI]00??FOZB

3.6.5 Tibia index

The tibia index is calculated with the following formula:

$$TI(t) = \left| \frac{M_R(t)}{(M_R)_C} \right| + \left| \frac{F_Z(t)}{(F_Z)_C} \right|$$

with:

$$M_R(t) = \sqrt{M_X(t)^2 + M_Y(t)^2}$$

Filtered Bending Moment M_x ??TIBI[LE,RI][UP,LO]??MOXB M_{x} ??TIBI[LE,RI][UP,LO]??FOZB F_z Filtered Force Fz $(M_R)_C$ 225Nm for HIII-50 & THOR, 115Nm for HIII-05, 306Nm for HIII-95

 $(F_z)_C$ 35.9kN for HIII-50 & THOR, 22.9kN for HIII-05, 44.1kN for HIII-95

4 VEHICLE & SLED CRITERIA CALCULATION

This section describes the calculation for each vehicle criteria including the filters that are applied (where applicable) to each channel used in these calculations. The analysis software used by the Euro NCAP labs will follow these calculations in detail.

4.1 Occupant load criterion

The calculation for the test vehicle and trolley OLC in the MPDB test is as follows.

Measured X-acceleration (A_X) on the centre of gravity of MPDB shall be filtered using CFC180.

The acceleration from the backup CoG accelerometer shall only be used for the OLC calculation where there is a channel failure of the primary accelerometer.

The filtered acceleration pulse shall be integrated with the following equation to derive the velocity course of the barrier:

$$V_t = \int A_X(t) \, dt + V_0$$

Where V_0 is the initial velocity at t = 0s.

 $\mathit{OLC}_{\mathit{SI-unit}},\,t_1$ and t_2 can be calculated with solving the following equation system:

$$\begin{cases} \int_{t=0}^{t=t_1} V_0 \ dt - \int_{t=0}^{t=t_1} V(t) \ dt = 0.065 \\ \int_{t=t_1}^{t=t_2} \left(V_0 - OLC_{SI-unit} \times (t-t_1) \right) dt - \int_{t=t_1}^{t=t_2} V(t) \ dt = 0.235 \\ V_0 - OLC_{SI-unit} \times (t_2-t_1) = V(t_2) \end{cases}$$

Where:

- t_1 is end of the free-flight-phase of a virtual dummy in vehicle or on the barrier along a displacement of 0.065m, and
- t_2 is end of the restraining-phase of a virtual dummy in vehicle or on the barrier along a displacement of 0.235m after the free-flight-phase (i.e. in total 0.300m displacement for the virtual dummy).

OLC shall be converted from SI units into g (standard gravity) with the conversion factor of $1g = 9.81 \text{m/s}^2$

4.2 Whiplash seatback dynamic deflection

The seatback dynamic deflection is defined as the maximum change in angle achieved at any time during the test between the T zero position and T-HRC(end). Measure the seatback dynamic deflection from the targets defined in the Euro NCAP Film and Photo protocol as follows:

- Define a line between the upper and lower seatback targets, ST2 and ST3.
- Define a second line between the forward and rearward sled base targets, B1 and B2.
- Calculate the angle between these two lines at the T-zero position. The instantaneous seatback deflection is defined as the instantaneous difference in angle between the T-zero position and the deflected position. Track the change in instantaneous angle between these two lines, throughout the dynamic test.

4.3 Compatibility criteria

$$CC = OLC_C + SD + BO$$

with:

$$OLC_C = \left\{ \begin{array}{ll} 0 & OLC \leq 25g \\ OLC_N * 25 & 25g < OLC \leq 40g \\ OLC > 40g \end{array} \right.$$

$$SD = \begin{cases} SD_N * 25 & OLC \le 25g \\ SD_N * ([25 + OLC_N * 75] - [OLC_N * 25]) & 25g < OLC \le 40g \\ SD_N * 75 & OLC > 40g \end{cases}$$

$$OLC_N = \frac{OLC - 25}{40 - 25}$$

$$SD_N = \frac{SD - 50}{150 - 50}$$

where:

CC Compatibility criteria in percentage

Occupant Load Criterion modifier based on the OLC of the MPDB trolley in g

Standard Deviation modifier based on the deformation of the PDB element

BO Bottoming-Out modifier based on the deformation of the PDB element

Please note, for the purposes of the compatibility modifier, data is required at a sampling rate of 20kHz. The calculation of velocity change (dV), a CFC of 180 shall be used.